

Yan Lin, Weekly report 07/05/05

General concept on fault tolerant computing

Measures of Fault-Tolerant Computing

i) Dependability: - a qualitative description that encompasses the terms above and reflects the overall quality of service.

ii) Reliability: $R(t)$ -- the probability that a system will function properly over the time interval $0 \dots t$. (Typical spacecraft requirement $R(10 \text{ years}) = 0.95$, aircraft requirement $R(10 \text{ hours}) = .999999999$)

iii) Availability: $A(t)$ -- the probability that a system is operating correctly and able to perform its function at time t . (Sometimes expressed differently -- maximum downtime in an interval, e.g. telephone system < 10 minutes in 40 years.)

iv) Performability: $P(L,t)$ the probability that a system will perform at or above some level L at time t . (Example a large network.)

v) Maintainability: $M(t)$, the probability that a failed system can be restored to working condition within time t .

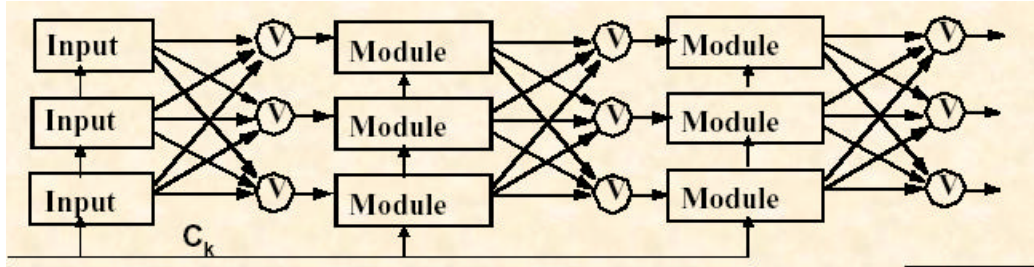
vi) Testability: -- the ability to test a system; often measured in test coverage (the percentage of faults of a given class that can be uncovered by the test procedure).

vii) Safety: $S(t)$ -- the probability that a system will either perform its functions correctly or fail in a benign way. (Example, a nuclear power plant).

Basic hardware redundancy techniques

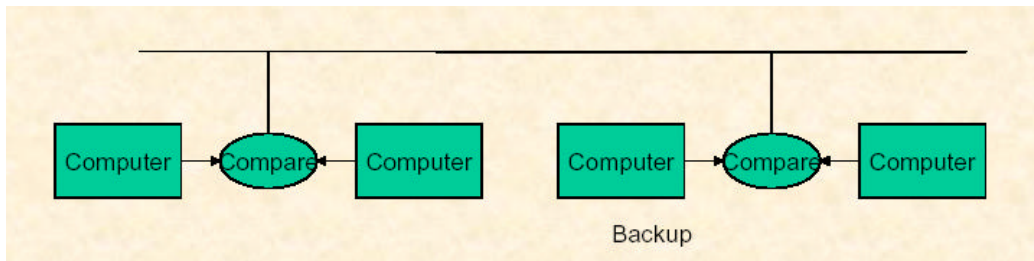
i) Replicate and Vote

Hardware-Implemented Triple Modular Redundancy (TMR)



ii) Duplicate and Compare

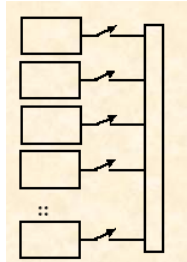
Duplex Self-Checking Approach (Stratus)



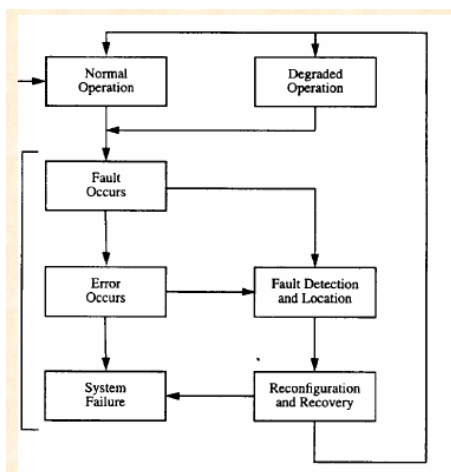
Computers run same programs in lockstep. If one pair internally disagrees, the other pair takes over immediately.

iii) Check and Replace (Standby Redundancy)

Active Hardware Redundancy – Detect error, remove fault, reconfigure, and recover state



basic operation of an active approach to fault tolerance



The Carter Self-checking Checker

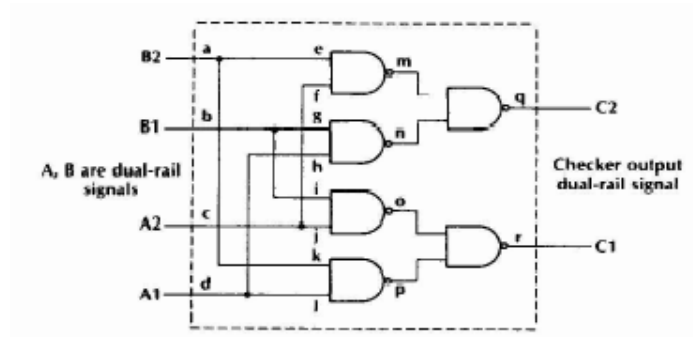
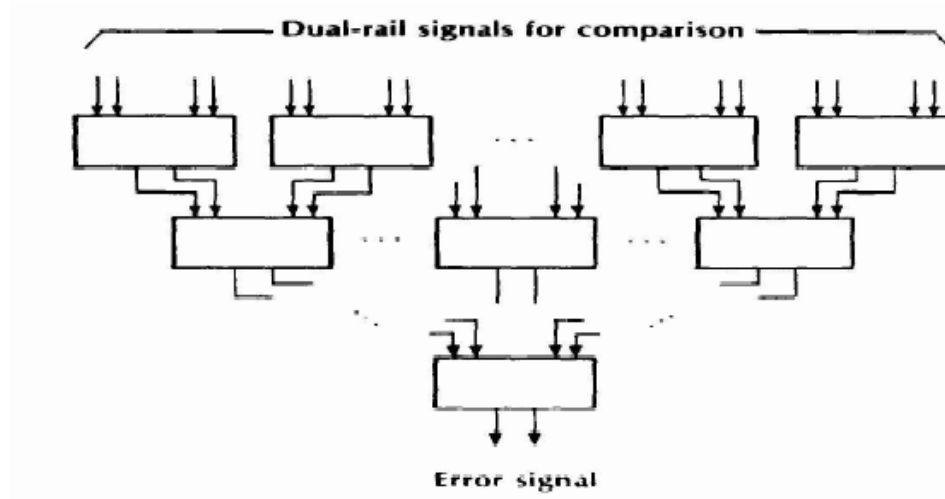


Table 3-12. TSC dual-rail comparator responses to stuck-at-faults.

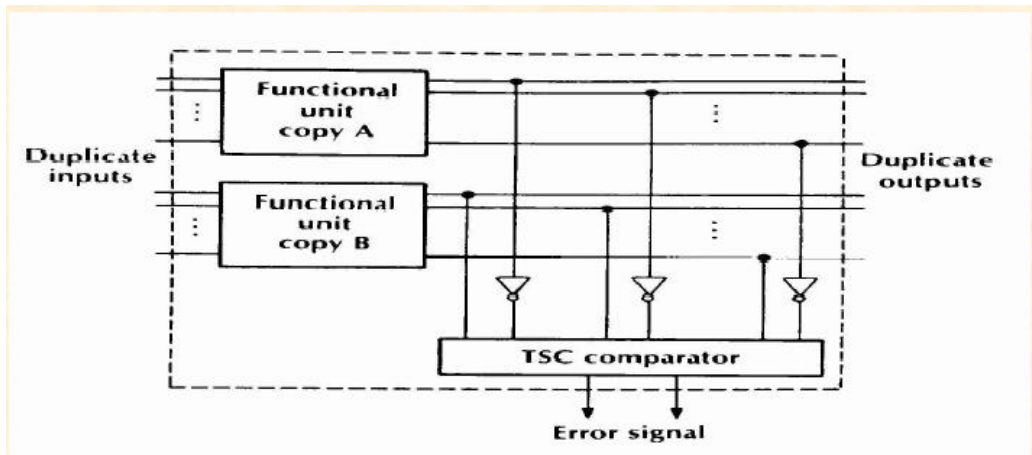
Inputs			Outputs C2C1 Resulting from Single Stuck-at-1 Faults																	
B2B1	A2A1	Normal Output	a	b	c	d	e	f	g	h	i	j	k	l	m	n	o	p	q	r
01	01	10	11	10	11	10	10	10	10	10	10	11	11	10	10	00	10	10	10	11
01	10	01	11	01	01	11	11	01	01	11	01	01	01	01	01	01	00	01	11	01
10	01	01	01	11	11	01	01	11	11	01	01	01	01	01	01	01	01	01	00	11
10	10	10	10	11	10	11	10	10	10	10	11	10	10	11	00	10	10	10	10	11

Inputs			Outputs C2C1 Resulting from Single Stuck-at-0 Faults																	
B2B1	A2A1	Normal Output	a	b	c	d	e	f	g	h	i	j	k	l	m	n	o	p	q	r
01	01	10	10	00	10	00	10	10	00	00	10	10	10	10	10	10	11	11	00	10
01	10	01	01	00	00	01	01	01	01	01	00	00	01	01	11	11	01	01	01	00
10	01	01	00	01	01	00	01	01	01	01	01	01	00	00	11	11	01	01	01	00
10	10	10	00	10	00	10	00	00	10	10	10	10	10	10	10	10	11	11	00	10

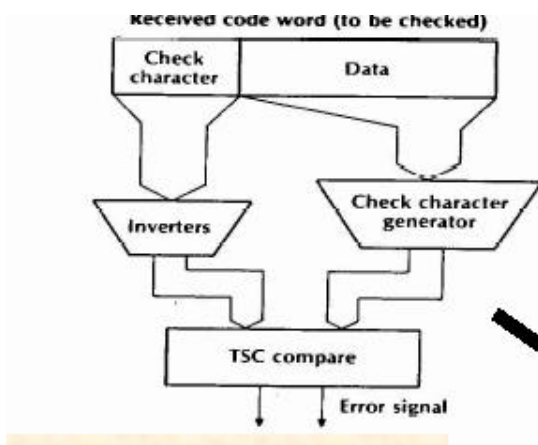
Assembly of n-input dual-rail signal comparison checker from basic two-input elements



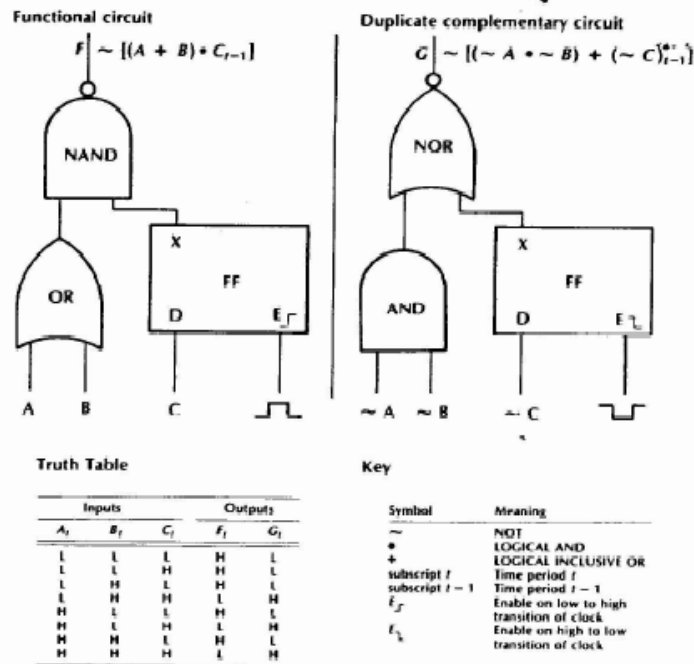
Self-checking circuit that duplicates and compares using a tree of Morphic And gates as below



Input protection

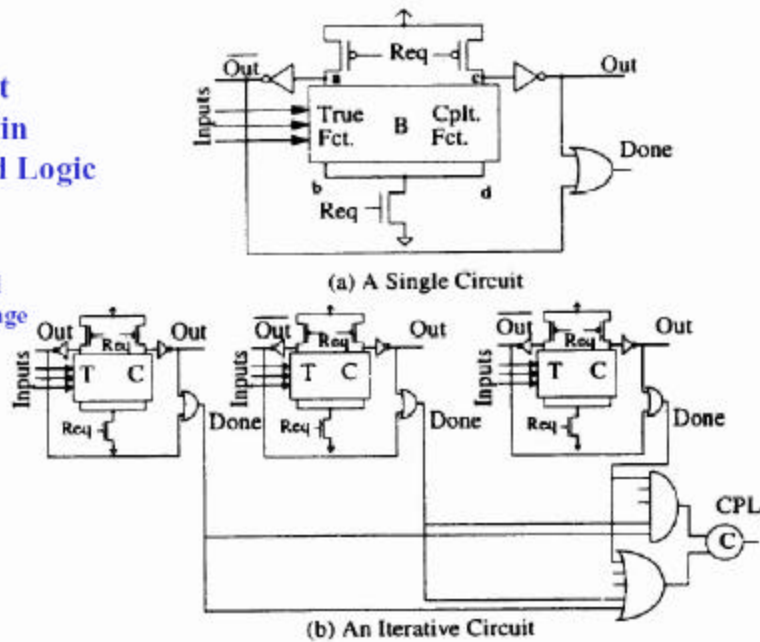


Using Complementary Logic to Detect Common Faults in a Duplicated System



Redundant Signaling in Self-Timed Logic

a) Differential Cascode Voltage Switch Logic (DCVSL)



- two wire logic 00 setup, 10,01 signal values, 11 error. Or of two wires signals completion

Basic Modeling

$R(t)$ = probability the system does not fail before time t , i.e., starting at $t=0$ the system provides acceptable service at least until time t .

If one was to create N identical systems, put them into service at $t=0$ and at time t group them into two subsets N_g (those still working) and N_f (those that have failed) then:

$N = N_g + N_f$, and in the limit as N goes to infinity

$$R(t) = \frac{N_g(t)}{N_g(t) + N_f(t)} = N_g(t)/N = 1 - N_f(t)/N \quad \text{and Unreliability } Q(t) = 1 - R(t) = N_f(t)/N = 1 - N_g(t)/N$$

$dR(t)/dt = d(1 - N_f(t)/N)dt = -(1/N) dN_f(t)/dt$ - this will decrease as a function of time because modules that failed cannot fail again.

We define the hazard function, or hazard rate, or failure rate function as

$$z(t) = (1/N_0(t)) dN_f(t)/dt = (1/N_0(t)) (-N) dR(t)/dt = \frac{dR(t)/dt}{R(t)} \quad \text{where } N_0(t) \text{ is the number of nodes remaining operational}$$

This is the instantaneous rate (per module) that failures are occurring among the remaining working modules.

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A non-redundant system with Constant Failure Rates

The Reliability function for Non-Redundant Systems

$dR(t)/dt = -z(t) R(t)$ if we assume that the failure rate is a constant λ then

$$dR(t)/dt = -\lambda R(t) \quad \text{which has the solution}$$

$$R(t) = e^{-\lambda t}$$

and if there are several independent components, all of which must work:

$$R(t) = R_1(t) * R_2(t) * R_3(t) \dots * R_m(t) \quad \text{then } R(t) = e^{-\lambda_1 t} * e^{-\lambda_2 t} * e^{-\lambda_3 t} \dots * e^{-\lambda_m t}$$

or $R(t) = e^{-(\lambda_1 + \lambda_2 + \lambda_3 \dots + \lambda_m)t}$ You just add the failure rates of the internal components

The constant failure rate is commonly used for most reliability modeling.

It's a reasonable approximation to reality and it is mathematically tractable.

Mean Time to Failure: MTTF

$$MTTF = \sum_{i=1}^N \frac{t_i}{N}$$

The *MTTF* can be calculated by finding the expected value of the time of failure. From probability theory, we know that the expected value of a random variable, *X*, is

$$E[X] = \int_{-\infty}^{\infty} xf(x)dx$$

where *f(x)* is the probability density function. In reliability analysis we are interested in the expected value of the time of failure (*MTTF*), so

$$MTTF = \int_{-\infty}^{\infty} tf(t)dt$$

$$= -\int_0^{\infty} t \frac{dR(t)}{dt} dt = \left[-tR(t) + \int R(t)dt \right]_0^{\infty} = \int_0^{\infty} R(t)dt$$

MTBF is simply the integral of the reliability function from 0 to infinity, and for non-redundant systems:

$$\int_0^{\infty} e^{-\lambda t} dt = \frac{1}{\lambda}$$

1.1 Basic Concepts of Combinational Reliability Models

For statistically independent events $P(A \text{ and } B) = P(A) * P(B)$

Given a system of *n* modules: $M(1), M(2), M(3), \dots, M(n)$,

and a reliability for each module: $R(1), R(2), R(3), \dots, R(n)$

where *R(i)* is the probability the *i*th module is OK

We perform an experiment to see which state the system is in.

There are 2^n possible outcomes:

W,W,W,.....,W,W $P(S1) = R(1) * R(2) * \dots * R(n-1) * R(n)$

W,W,W,.....,W,F $P(S2) = R(1) * R(2) * \dots * R(n-1) * (1-R(n))$

W,W,W,.....,F,W $P(S3) = R(1) * R(2) * \dots * (1-R(n-1)) * R(n)$

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F, F, F,,F, F $P(S2^n) = (1-R(1)) * (1-R(2)) * \dots * (1-R(n-1)) * (1-R(n))$

To determine the reliability of a redundant system simply sum the probabilities of being in a working configuration.

If the system can tolerate two module failures, add the first three probabilities

$P(S1\text{-all work}) + P(S2\text{-all but one work}) + P(S3\text{-all but two work})$ etc.

The Concept of Coverage

Coverage “*c*” is defined as the conditional probability, given that a fault occurs, that the system will be able to recover from it.

It is a measure of the “goodness” of the fault-tolerance features of a system. We shall see that it is the most important (sensitive) parameter in determining the reliability of fault-tolerant systems.

Expanding the combinational models to include coverage:

Going back to the basic concept of listing outcomes and summing those that correspond to a working system:

$$\begin{aligned}
 W, W, W, \dots, W, W & P(S1) = R(1) * R(2) * \dots * R(n-1) * R(n) \\
 W, W, W, \dots, W, F & P(S2) = R(1) * R(2) * \dots * R(n-1) * (1-R(n)) \\
 W, W, W, \dots, F, W & P(S3) = R(1) * R(2) * \dots * (1-R(n-1)) * R(n) \\
 \vdots & \vdots \\
 F, F, F, \dots, F, F & P(S2^n) = (1-R(1)) * (1-R(2)) * \dots * (1-R(n-1)) * (1-R(n))
 \end{aligned}$$

For all cases where an active computer fails there are now two cases -- one multiplied by c -- the probability of correct recovery and one multiplied by $(1-c)$ the probability of incorrect recovery. Only the correctly recovered outcome can be counted.

This gets a bit complicated since failures of spares that are never called upon to replace active units have no coverage associated with their failure.

Consider a system with one active units and two spares: (The left unit starts as the active unit and spares are selected for replacement going from left to right.)

$$R = p(WWW) + c * p(FWW) + p(WFW) + p(WWF) + p(WFF) + c * p(FWF) + c * c * p(FFW)]$$

of course $p(FFF)$ is excluded but what are the assumptions in including $p(FFW)$?

MARKOV MODELS

CONSIDER OUR NON-REDUNDANT SYSTEM:

$$R(t+dt) - R(t) = -R(t) * \lambda dt$$

$$\frac{dR(t)}{dt} = -\lambda * R(t) \rightarrow R(t) = e^{-\lambda t}$$



LET'S EXTEND THIS TO A SUBSYSTEM WITH 3 MODULES

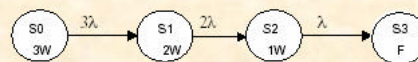
S0: ALL THREE MODULES WORK

S1: ONE HAS FAILED, TWO WORK

S2: TWO HAVE FAILED, ONE WORKS

S3: ALL HAVE FAILED

Yields the following State Diagram



AND THE CORRESPONDING SET OF DIFFERENTIAL EQUATIONS

$$\begin{bmatrix} dP0 \\ dP1 \\ dP2 \\ dP3 \end{bmatrix} = \begin{bmatrix} -3\lambda & 0 & 0 & 0 \\ +3\lambda & -2\lambda & 0 & 0 \\ 0 & +2\lambda & -\lambda & 0 \\ 0 & 0 & +\lambda & 0 \end{bmatrix} \begin{bmatrix} P0 \\ P1 \\ P2 \\ P3 \end{bmatrix}$$

Start with $P0, P1, P2, P3 = 1, 0, 0, 0$