Weekly Report for Yu Hu's work from Aug. 29 to Sep. 4

September 4, 2005

1 Prove the line case of level converter free formulation

1.1 Model and formula

The line case (see Figure 1) in King Ho's DAC'05 paper is used in our proof. The logic of the proof is that, whenever the first level converter is used (low V_{dd} buffer drives high V_{dd} buffer), we can always switch the high V_{dd} buffer and low V_{dd} buffer while keeping the optimal power under the given timing constraint.



Figure 1: Comparison cases for the proof

In Figure 1, we assume $l_1 + l_2 = p_1 + p_2 = L$. Under a certain technical node, we can always assume that the settings (input capacitance C_{in}^0 , intrinsic delay D_{int}^0 and output resistance R_d^0) min-size buffer are given. We set the size of low V_{dd} buffer , high V_{dd} buffer and level converter in case (A) as x, y and z, and the size of low V_{dd} buffer in case (B) as u and w. Based on these constant parameters, we calculate the Elmore delay of case (A) and (B) as follows.

$$Delay_{A} = R_{in}C_{L} + D_{L} + R_{L}(c_{w} + l_{1} + C_{LC}) + r_{w}l_{1}(c_{w}l_{1}/2 + C_{LC}) + D_{LC} + R_{LC}C_{H} + D_{H} + R_{H}(c_{w}l_{2} + C_{load}) + r_{w}l_{2}(c_{w}l_{2}/2 + C_{load})$$

$$Delay_{B} = R_{in}C'_{H} + D'_{H} + R'_{H}(c_{w}p_{1} + C'_{L}) + r_{w}l_{1}(c_{w}p_{1}/2 + C'_{L}) + (1)$$

$$D'_{H} + R'_{L}(c_{w}p_{2} + C_{load}) + r_{w}p_{2}(c_{w}p_{2}/2 + C_{load})$$
(2)

where

Power dissipation by case (A) and (B) can be calculated as follows.

$$Power_{A} = x \cdot E_{L} + y \cdot E_{L} + z \cdot E_{LC} + 0.5 \cdot c_{w} \cdot l_{2} V_{dd}^{H^{2}} + 0.5 \cdot c_{w} \cdot l_{1} V_{dd}^{L^{2}}$$
(3)

$$Power_B = u \cdot E_L + w \cdot E_L + 0.5 \cdot c_w \cdot p_1 V_{dd}^{H^2} + 0.5 \cdot c_w \cdot p_2 V_{dd}^{L^2}$$
(4)

Obviously, the power dissipation of case (A) and (B) might be sensitive to min-size buffer settings, buffer size, V_{dd} level, and timing constraints etc. Now I'm going to show the effect of the above parameters to the difference of power between (A) and (B). A typical global wire length is selected in the following analysis since the results are scalable based on the wire length.

1.2 Effect of timing constraints

Firstly, I'll show the effect of timing constraint on power dissipation. Under the typical settings of min-buffer and V_{dd} level in 65nm technical node, the power of (A) and (B) under the timing constraints from the optimal delay to 110% optimal delay is shown in Figure 2. It's easy to find that $Power_A$ is much larger than $Power_B$ when the timing constraint is tight, $Power_A$ becomes close to $Power_B$ when timing constraint is looser, and ultimately the difference between $Power_A$ and $Power_B$ is a constant as power is totally decided by V_{dd} level and min-buffer size under over-loosed timing constraint. The most important part is that $Power_A$ is always larger than $Power_B$ under the same timing constraint. To exclude the effect of V_{dd} level on the result, I tested two groups of V_{dd} settings. Figure 2 shows that the results under both V_{dd} levels are consistent.



Figure 2: Slack vs. Power

1.3 Effect of upstream res and downstream cap

Then, I'll show the effect of upstream resistance R_{in} and the downstream load capacitance C_{load} on power dissipation of (A) and (B). The R_{in} and C_{load} are set to be from 1x to 1000x resistance and capacitance of the min-size buffer, respectively. Also three kinds of timing constraints, such as optimal delay, 10% slack and 50% slack, are used respectively. Figure 3 shows the results. We can find that $Power_A$ is always larger than $Power_B$ when C_{load} is less than 700x capacitance of the min-size buffer. Actually, this is a reasonable assumption in our design as the downstream buffering can bound the load capacitance very well.

1.4 Effect of min-size buffer settings

At last, I'll show the effect of the output resistance R_D^0 and intrinsic delay D_{int} of the min-size buffer (we can treat the input capacitance of the min-size buffer as a constant in practice). R_D^0 is set to be from 50 Ω to 10000 Ω ,



Figure 3: R_{in} and C_{load} vs. Power

and D_{int} is from 10ps to 1000ps. The optimal delay, 10% and 50% slack timing constraints are tested. The results are shown in Figure 4, whose Z axe is $\frac{Power_A - Power_B}{Power_B}$ and x, y axes are R_D^0 and D_{int} respectively. We can find that $Power_A$ is always larger than $Power_B$ in this range.



Figure 4: R_D^0 and D_{int} vs. Power

1.5 A sufficient condition for the level converter free formulation

Thereom Given x-size low V_{dd} buffer and y-size high V_{dd} buffer in case (A), if we can always find a proper segments p_1 and p_2 to satisfy the timing constraint with simply switching these two buffers (without changing buffer sizes), then we have $Power_A > Power_B$ if $\beta \ge \frac{\alpha y+x}{2}$, where β is a ratio of the size of the wire L we considered comparing to the min-size buffer.

Proof We can write the resistance and capacitance by those of min-size buffer. Without losing generality, we ignore the constant coefficients and the Res and Cap of the wire l can be written as βR_d^0 and $\beta C_i^0 n$. For the level converter, we can simply treat it as $\alpha \times$ high V_{dd} buffer. In the other hand, the timing constraints $Delay_A \leq T$, $Delay_B \leq T \Leftrightarrow Delay_A - T = 0$, $Delay_B - T = 0$ for power optimization. We can substitute βR_d^0 , $\beta C_i^0 n$ and the buffer sizes in Eq.1 and Eq.2 and divide $C_i^0 n \cdot R_d^0$ in both sides and ignore all constant coefficients, then rearrange and get the following equations.

$$\beta_1^2 + \beta_1 \cdot (1/x + \alpha y - \beta - 1) + (1 + x + \alpha y/x + 1/\alpha + (\beta + 1)/y + \beta^2/2 + \beta - T) = 0$$
(5)

$$\gamma_2^2 + \gamma_2 \cdot (1/x - \beta + 1 - 1/y - x) + ((\beta + x)/y + \beta x + y + 1/x + \beta^2/2 - T) = 0$$
(6)

 \Rightarrow

$$\beta_{1} = \frac{-(1/x + \alpha y - \beta - 1) + \sqrt{(1/x + \alpha y - \beta - 1)^{2} - 4(1 + x + \alpha y/x + 1/\alpha + (\beta + 1)/y + \beta^{2}/2 + \beta - T)}}{2}$$

$$= \frac{B + \sqrt{B^{2} - 4C}}{2}$$
(7)

$$\gamma_{2} = \frac{-(1/x - \beta + 1 - 1/y - x) + \sqrt{(1/x - \beta + 1 - 1/y - x)^{2} - 4((\beta + x)/y + \beta x + y + 1/x + \beta^{2}/2 - T)}}{2}$$

$$= \frac{B' + \sqrt{B'^{2} - 4C'}}{2}$$
(8)

where β_1 and γ_2 is similar defined as β and T is the timing constraint divided by some constant. A sufficient condition for $\beta_1 < \gamma_2$ is that we have the following inequations.

$$B - B' = -(1/x + \alpha y - \beta - 1) - (-(1/x - \beta + 1 - 1/y - x)) = 2 - 1/y - x - \alpha y < 0$$
(9)

$$(B^{2} - 4C) - (B'^{2} - 4C') = \alpha^{2}y^{2} + 2\alpha y/x - 2\alpha y\beta - 2\alpha y + 2\beta - 4(1 + x) - 4\alpha y/x - 4/\alpha - 4(\beta + 1)/y - x^{2} - 1/y^{2} + 2/(xy) + 2 + 2\beta + 2(\beta + 1)/y + 2(\beta + 1)x + 2x/y + 4y \approx \alpha^{2}y^{2} - 2\alpha y\beta + 2\beta - x^{2} + 2\beta + 2(\beta + 1)x = \alpha^{2}y^{2} - x^{2} - (2\alpha y - 4 - 2x)\beta < 0 \Rightarrow \beta > \frac{\alpha^{2}y^{2} - x^{2}}{2\alpha y - 2x - 4} > \frac{(\alpha y - x)(\alpha y + x)}{2(\alpha y - x)} = \frac{\alpha y + x}{2}$$
(10)

Based on Eq.3 and Eq.4, the power of (A) and (B) can be written as follows with ignoring all constant coefficients.

$$pwr_A = x + (1+\alpha)y + V_H\beta_2 + V_L\beta_1 \tag{11}$$

$$pwr_B = x + y + V_H \gamma_1 + V_L \gamma_2 \tag{12}$$

$$\Rightarrow$$
 (13)

$$pwr_A - pwr_B = \alpha y + (V_L - V_H)(\beta_1 - \gamma_2)$$
(14)

Obviously, if $\beta_1 < \gamma_2$ then $pwr_A > pwr_B$.