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# Simultaneous Signal and Power Routing Based on Interconnect Estimation \*

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## Abstract

In this paper, we study the min-area simultaneous signal and power routing problem under a given noise bound (i.e., the SPR/NB problem). The resulting SPR/NB solution is free of capacitive noise, and satisfies a given inductive noise bound under the  $K_{eff}$  model. We first develop the pre-routing area estimation techniques for the min-area simultaneous shield insertion and net ordering (SINO) solutions. We then propose a two-phase approach to solve the min-area SPR/NB problem: in the first phase, we define a regular power/ground (P/G) structure according to the above area estimation; and in the second phase, we carry out SINO procedures to search for the best SPR/NB solution in a very limited neighborhood of the pre-defined P/G structure. Experimental results show that our approach is able to efficiently achieve the min-area SPR/NB solution by searching only the first-order neighborhood of the pre-defined P/G structure. Our ongoing work extends the interconnect estimation and two-phase SPR/NB algorithm to an explicit RLC noise model.

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# 1 Introduction

Given the growing importance of interconnects in performance, reliability, cost, and power dissipation for high-performance and power-efficient circuits and systems, the interconnect synthesis becomes a critical design aspect [1, 2]. Even though most existing interconnect synthesis work use the RC model, it becomes evident that the RLC model becomes more appropriate as the on-chip inductive effect gains increasing prominence in gigahertz designs [3].

Several work have considered interconnect optimization under RLC model for multiple coupled nets. In [4], a simultaneous shield insertion and net ordering (SINO/NB- $k$ ) problem was solved to find a min-area solution under the inductive coupling constraint using a  $K_{eff}$  model. Later on, a twisted-bundle layout scheme [5] was proposed to minimize the inductive coupling. Assuming that the current will return from the nearest shield, the loop inductance model is used in [4, 5]. However, the assumption is not true in general. Let a *block* denote the set of wires between two shields. The current often returns from quiet wires within a block if there are plenty of quiet wires in the current block. On the other hand, the current often returns from shields or quiet wires outside the current block when multiple wires in the current block switch simultaneously. A very recent work [3] removes the above assumption about the current return path. A table-based partial inductance model [6, 7] is adopted without pre-assuming any current return path, and a coupling inductance screening rule [8] is employed to decide the scope of the current return path (i.e., the scope of inductive coupling). Further, different from the  $K_{eff}$  model used as a figure of merit for the noise bound in [4] and no noise bound considered in [5], a high-order RLC noise model is developed in [3] to compute the peak noise voltage for multiple coupled RLC interconnects. Then, the min-area simultaneous shield insertion and net ordering (SINO/NB- $v$ ) problem is solved under the RLC noise model.

The above two SINO formulations, however, do not consider pre-routed power/ground (in short, P/G) structures. As P/G wires are also shields to reduce the inductive and capacitive noise, the number of shields needed by the two SINO algorithms depends on the pre-routed P/G structure (see Table 1 later on). Neither is it clear how to define the best P/G structure, and how to use the above two SINO formulations in the current global routing flow with pre-routed regular P/G wires.

As a first step to solve these concerns, especially on how to define the best P/G structure, we study in this paper the min-area simultaneous signal and power routing (SPR/NB) problem for given noise constraints. Our contributions include: (i) We develop simple yet accurate formulae to estimate the total number of shields needed by SINO/NB- $k$  solutions without running SINO algorithms. (ii) We develop an efficient algorithm for a new SINO problem (herein refer to as the  $p$ -SINO/NB- $k$  problem) with respect to the pre-routed P/G structure. (iii) We propose a two-phase solution to the min-area SPR/NB problem under the  $K_{eff}$  model: we first define a regular P/G structure according to the above area estimation, and then carry out  $p$ -SINO/NB- $k$  procedures with respect to the defined P/G structure and its first-order neighborhood. Experiments show that our two-phase approach is able to efficiently achieve the min-area SPR solution which satisfies the given noise bound and has a regular P/G structure.

The rest of this paper is organized as follows: Section 2 reviews the related work and presents the formulation and solution of the new  $p$ -SINO/NB- $k$  problem considering pre-routed P/G structures. Section 3 derives formulae for pre-SINO/NB- $k$  estimations, and formulate and solve the new SPR/NB- $k$  problem (i.e., the SPR/NB problem under the  $K_{eff}$  model). Section 4 concludes the paper, with discussions of ongoing and future works.

## 2 $p$ -SINO/NB- $k$ Formulation and Solution

### 2.1 Review of Previous SINO Work

According to [3, 4], we denote a signal net as  $s$ -wire, and define that two nets  $s_1$  and  $s_2$  are *sensitive* to each other, if a switching signal on  $s_1$  will cause  $s_2$  to malfunction (due to extraordinary crosstalk or delay variation) and vice-versa. In this case,  $s_1$  is an *aggressor* for  $s_2$ , and  $s_2$  a victim of  $s_1$ . The *sensitivity rate* of  $s_i$  is defined as the ratio of the number of aggressors for  $s_i$  to the total number of nets. The sensitivity for all s-wires in a given problem can be represented compactly with a sensitivity matrix  $S$  of size  $n \times n$ , where  $n$  is the number of s-wires. An entry of 1,0 in location  $(i, j)$  indicates that  $s_i$  and  $s_j$  are sensitive or not sensitive, respectively, to one another. A *shield* is a wire directly connected to P/G wires. We use the terms “wire” and “net” interchangeably in this paper. Inserting a shield between two sensitive s-wires is able to eliminate the capacitive coupling and reduce the inductive coupling.

The simultaneous shield insertion and net ordering (*SINO*) problem has been studied under the  $K_{eff}$  model in [4], and under explicit RLC noise constraint in [3]. As an SINO solution can be viewed as a *placement* of shields and signal nets to routing tracks, an SINO solution can be also called a placement. Then, the noise bounded SINO problem under the  $K_{eff}$  model (the SINO/NB- $k$  problem) is defined as:

**Formulation 1** (*Optimal SINO/NB- $k$  problem*): For a given placement  $P$ , find a new placement  $P'$  with minimum area by simultaneous shield insertion and net re-ordering such that any  $s_i$  in  $P'$  is free of capacitive noise and its inductive coupling is less than a given bound using the  $K_{eff}$  model.

The noise bound in the the SINO/NB- $k$  problem is given by the  $K_{eff}$  model, but not a noise voltage that is most intuitive and convenient to the designer. Additionally, the SINO/NB- $k$  problem does not allow placing a victim adjacent to an aggressor, and may lead to over-design in practice. A more general SINO/NB- $v$  problem is formulated as follows [3]:

**Formulation 2** (*Optimal SINO/NB- $v$  problem*): For a given placement  $P$ , find a new placement  $P'$  with the minimum area by simultaneous shield insertion and net re-ordering such that the peak noise of any wire  $s_i$  in  $P'$  satisfies the given explicit noise constraint for wire  $s_i$ .

A high-order RLC circuit model is developed in [3] to compute the peak noise that can be induced for the victim over all signal patterns of its aggressors. The partial inductance model [6] is used without assuming any current return path, and a wire is modeled in general by multiple RLC segments. Coupling capacitance is considered only for adjacent wires, while coupling inductance is considered for any two wires. Table-based models presented in [7] and [9] are used to obtain the capacitance and inductance. The scope of mutual inductance is decided by a screening rule [8, 3].

Compared to the RLC noise model, the  $K_{eff}$  model is less intuitive and convenient to the designer. However, it is easy to compute and has a high fidelity versus the SPICE-computed RLC noise voltage. As shown in [10], a SINO/NB- $k$  solution that has a higher coupling value under the  $K_{eff}$  model also has a higher SPICE-computed noise voltage using the table-based RLC circuit model. Therefore, we study in this paper the interconnect estimation and the simultaneous signal and power routing (*SPR*) problem, both under the  $K_{eff}$  model. Our ongoing work extends the interconnect estimation and SPR problem to the explicit RLC noise model, as discussed in Section 4 of this paper.

## 2.2 $p$ -SINO/NB- $k$ Formulation

Note that pre-routed P/G wires are also shields in the sense that they can eliminate the capacitive coupling and reduce the inductive coupling, but were not considered in [3, 4]. For differentiation, we call shields in [3, 4] as  $g$ -wires (or *movable shields*) that can be placed at any routing track in contrast to those pre-routed P/G wires (or *fixed shields*). In order to consider pre-routed P/G structures that are widely used in the current global routing flow, we formulate the new  $p$ -SINO/NB- $k$  problem as follows:

**Formulation 3** (*Optimal  $p$ -SINO/NB- $k$  problem*): For a given placement  $P$  with pre-routed P/G structure, find a new placement  $P'$  with the minimum area by simultaneous shield ( $g$ -wire only) insertion and net re-ordering such that any  $s_i$  in  $P'$  is free of capacitive noise and its inductive coupling is less than a given bound using the  $K_{eff}$  model.

For the simplicity of presentation, we assume that an SINO solution is found where the inductive coupling for each net meets the given noise bound under the  $K_{eff}$  model. We also assume that the P/G structure is regular, i.e., the *pitch space*, defined as the number of tracks between a pair of adjacent P/G wires, is a constant. In this formulation, only a signal net or a movable shield can be assigned to an arbitrary routing track.

## 2.3 $p$ -SINO/NB- $k$ Algorithm

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Simulated Annealing Algorithm: Given a placement  $P$ :
Repeat
     $Temp = \text{Initial\_Temperature}$ ;
    Schedule Random_Move( $P, P'$ );
         $Candidate\_Cost = \text{Compute\_Cost}(P')$ ;
         $ds = Candidate\_Cost - \text{Compute\_Cost}(P)$ ;
        if ( $ds < 0$ )
             $P = P'$ ;
        else
             $r = \text{RANDOM}(0, 1)$ ;
            if ( $r < \exp(-ds/Temp)$ )
                 $P = P'$ ;
    Until equilibrium at  $Temp$  is reached;
     $Temp = Temp * \text{Temperature\_Adjustment}$ ;
    /*( $0 < \text{Temperature\_Adjustment} < 1$ )*
Until  $Temp == \text{Freezing\_Point}$ ;

```

Figure 1: Framework of simulated annealing algorithms for SINO/NB- $k$  and  $p$ -SINO/NB- $k$  problems

It has been proved in [3, 4] that the optimal SINO/NB- $k$  and SINO/NB- $v$  problems are NP-hard, and heuristic methods have been developed to obtain high quality solutions with reasonable computational time. Figure 1 gives the framework of the simulated annealing algorithms used in [3] for the SINO/NB- $k$  problem and in this paper for the  $p$ -SINO/NB- $k$  problem. As highlighted in Figure 1, the two algorithm are different in terms of the random moves and scheduling scheme. The random moves performed by [3] are:

### Random Moves for SINO/NB- $k$ problem

- (i) Combine two random blocks in  $P$ . If the two random blocks are adjacent, this is equivalent to removing a g-wire. Removing a g-wire can be done by shifting left all its right-handed wires.
- (ii) Insert a g-wire at a random track in  $P$  by shifting right all wires which are to the right of this track.
- (iii) Move a single random s-wire to a new and random track, this should be done in two steps:
  - (a) Remove this net from its original track, and shift left by one track all right-handed wires, ranging from this net's original track to the new random track,
  - (b) Insert this net to the new and random track by shifting right all wires which are to the right of this track,
- (iv) Swap two random s-wires in  $P$ .

The SINO/NB- $k$  problem does not have pre-routed P/G structures and *all* shields can be moved freely. However, for the new  $p$ -SINO/NB- $k$  problem, only g-wires can be moved during the simulated annealing procedure, but all P/G wires are assigned to *fixed* tracks. The above difference leads to more sophisticated random moves as follows:

### Random Moves for $p$ -SINO/NB- $k$ problem

- (i') Combine two adjacent blocks divided by a g-wire by removing this g-wire, and shift left by one track all its right-handed s-wires and g-wires (but not P/G wires),
- (ii') Insert a g-wire at a random track in  $P$  by shifting right all s-wires and g-wires (but not P/G wires) which are to the right of this track,
- (iii') Move a single random s-wire to a new track not occupied by the P/G wire, this should also be done in two steps:
  - (a) Remove this s-wire from its original track, and shift left by one track all right-handed wires except P/G wires, ranging from this s-wire's original track to the new random track,
  - (b) Insert this s-wire to the new and random track by shifting right all s-wires and g-wires (but not P/G wires) which are to the right of this track,
- (iv') Swap two random nets in  $P$ .

Note that moves (i)-(iv) can be viewed as local moves in the solution space for the SINO/NB- $k$  problem, but the new moves (i')-(iii') may be no longer local moves in the solution space for the  $p$ -SINO/NB- $k$  problem. The simple scheduling scheme, performing random moves with equal weights for the SINO/NB- $k$  problem, will lead to too many rejections for the  $p$ -SINO/NB- $k$  problem. To reach a satisfactory solution with as few rejections as possible for the  $p$ -SINO/NB- $k$  problem, we iterate through random moves (i')-(iv') with different weights. We always use more move (iv') than other moves. But as the temperature decreases, the number of move (iv') becomes smaller. Moves which create two adjacent shields in the placement are categorically rejected and a new move is tried. The starting temperature, freezing point, temperature adjustment and variance threshold factors are all determined experimentally, but are fixed for all experiments on SPR/NB- $k$  solutions to be presented in the next section.

sensitivity rate	pitch size of P/G structures					
	7	8	9	10	11	12
30%	7.6/3.6	7.0/3.0	8.4/5.4	6.2/3.2	<b>4.0/2.0</b>	4.8/2.8
50%	8.2/4.2	7.4/3.4	6.6/3.6	<b>5.4/2.4</b>	5.8/3.8	5.2/3.2
70%	8.8/4.8	<b>6.2/2.2</b>	8.8/5.8	7.8/4.8	7.4/5.4	6.6/4.6

Table 1: Summary of  $p$ -SINO/NB- $k$  solutions for 32 signal nets with uniform sensitivity rates. In each cell of column 2-7 in the table, the first value is the total number of shields, and the second value is the total number of g-wires. The  $K_{thresh}$  is 1.0.

sensitivity rate	pitch size of P/G structures					
	7	8	9	10	11	12
30%	0.63/0.48	0.69/0.52	0.66/0.43	0.70/0.51	0.79/0.57	0.76/0.52
50%	0.62/0.45	0.65/0.47	0.73/0.54	0.80/0.55	0.76/0.51	0.84/0.57
70%	0.65/0.47	0.83/0.54	0.67/0.46	0.72/0.41	0.77/0.53	0.81/0.53

Table 2: Maximum and average coupling values for  $p$ -SINO/NB- $k$  solutions with different pitch sizes. In each cell of column 2-7 in the table, the first value is the maximum coupling, and the second value is the average coupling.

## 2.4 Experimental Results

We have implemented an integrated toolset in the C/C++ programming language. The toolset includes the table-based models for capacitance and inductance proposed in [7] and [9], all shields insertion and net ordering algorithms proposed in [3, 4] and this paper, and SPICE net list generation. The SPICE net list can be automatically generated and be used to verify the interconnect optimization result. We have tested our algorithm and implementation using a large number of random examples. We generate ten different sensitivity matrices and initial placement for each design combination of P/G structure and sensitivity rate. For this sub-section, the sensitivity rates range from 30% to 70% and these sensitive nets are picked randomly for a given s-wire. The inductive noise bound  $K_{thresh}$  is set to 1.0. Note that the  $K_{eff}$  model is independent of the width, length, and spacing of s-wires and g-wires, as illustrated in [11].

We present experimental results for various test cases for 32 signal nets in this sub-section. The average number of shields is summarized in Table 1, and the maximum and average coupling for the resulting  $p$ -SINO/NB- $k$  solutions in Table 2. From Table 2, one can easily see that all maximum coupling values are smaller than 1.0, so that all  $p$ -SINO/NB- $k$  solutions meet the specified noise bound  $K_{thresh}$ . Further, as shown in Table 1 where the min-cost solution is highlighted for each sensitivity rate, different P/G structures (i.e., different P/G pitch spaces) lead to SINO solutions with different costs. For example, in the case of 30% sensitivity rate, the best P/G structure has a P/G pitch space of 11 and leads to a min-area solution with total 4.0 shields on average. On the other hand, decreasing the P/G pitch space to 10 leads to total 6.2 shields on average, an increase of more than 50% compared to the min-area solution. This observation motivates us to study the simultaneous power and signal routing (SPR/NB) problem to find the best P/G structure that can achieve the min-area solution in the next section.

### 3 SPR/NB- $k$ Formulation and Solution

To find the min-area SINO solution with a regular P/G structure, we define the following simultaneous signal and power routing (*SPR/NB- $k$* ) problem under the  $K_{eff}$  model:

**Formulation 4 (min-area SPR/NB- $k$  problem)** *For a number of signal nets and a given inductive coupling constraint, the min-area SPR/NB- $k$  problem decides a regular P/G structure, assigns signal nets to routing tracks, and insert necessary g-wires (i.e., movable shields), such that the resulting SPR solution has a minimum area, and has g-wires fewer than P/G wires. Further, any s-wire in the SPR solution is free of capacitive noise and its inductive noise is less than the given bound under the  $K_{eff}$  model.*

Because g-wires have to be connected with P/G wires, g-wires (movable shields) bear implicit routing overhead and may alleviate the desired regularity of P/G structures. Therefore, a good SPR/NB solution should have as few g-wires as possible, and we explicitly require that g-wires be fewer than P/G wires in our problem formulation, i.e., on average, there is at most one g-wire inserted between every pair of adjacent P/G wires. In the following, we will first develop the pre-SINO/NB- $k$  area estimation, then propose a two-phase SPR/NB- $k$  solution based on this area estimation.

#### 3.1 Pre-SINO Estimation for SINO/NB- $k$ Solutions

We first introduce the formula for the numbers of shields needed by the SINO/NB- $k$  problem with uniform sensitivity, where each net has the same sensitivity rate. We show later on that this formula can be applied to the non-uniform sensitivity case with modest modifications. In the rest of this paper, we denote the number of shields as  $N_s$ , the number of nets  $N$ , and uniform sensitivity rates  $S$ .

N	sensitivity rate			
	20%	40%	60%	80%
16	3.0	3.8	4.5	5.0
32	4.0	5.6	6.8	8.0
64	6.6	10.0	13.0	14.8

Table 3: Numbers of shields needed by the SINO/NB- $k$  problem with  $K_{thresh} = 1.0$

##### 3.1.1 RLC Nets with Uniform Sensitivity Rates

From Table 3, we can know that the number of shields should be a monotonous increasing function of the number of RLC nets and uniform sensitivity rates. Figure 2 also shows that given the fixed value of sensitivity rates, the number of shields is a linear function of the number of nets with two unknown parameters:

$$N_s = a_1 \cdot N + b_1 \tag{1}$$

and given the fixed number of nets, the number of shields is a two-order polynomial function of the uniform sensitivity rates with three unknowns:

$$N_s = a_2 \cdot S^2 + b_2 \cdot S + c_2 \tag{2}$$

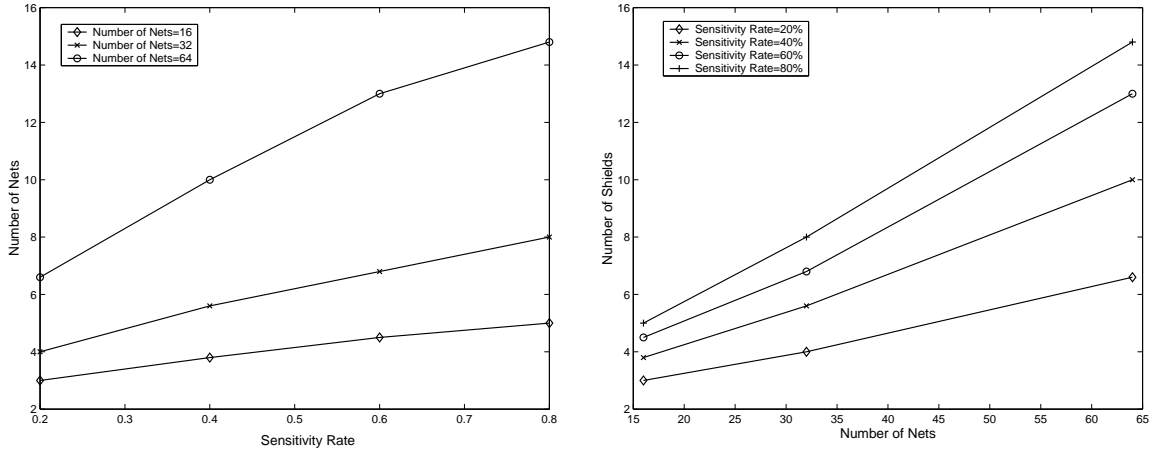


Figure 2: The function for the number of shields is linear with respect to the number of nets, and is two-order polynomial with respect to the sensitivity rate.

parameter	final estimate	standard error	probability
a	-0.175343189	0.07760582	0.03580
b	1.1988973	3.153509	0.80803
c	0.378187878	0.07815248	0.00011
d	-0.341193692	3.175723	0.91557
e	0.0212514404	0.01713278	0.22993
f	0.806603546	0.6961897	0.26098

Table 4: Calculated parameters values

Considering the two one-variable functions (1) and (2), parameters in one function can in fact be represented by the other function. Thus we replace the parameters in either function with the form of the other function. In this work, we obtain the following function by representing the three parameters in function (2) with function (1) as follows:

$$N_s = (a \cdot N + b) \cdot S^2 + (c \cdot N + d) \cdot S + e \cdot N + f \quad (3)$$

We use a nonlinear regression analysis method [12, 13] to obtain the value (see Table 4) for these parameters. The rightmost column of the table shows the probability of that parameter to be zero. For the formula's simplicity without loss of accuracy, we omit the terms whose coefficients have more than 80% possibility to be zero. The final formula for the numbers of shields with respect to  $K_{thresh} = 1.0$ , the uniform sensitivity rates, and the number of nets is:

$$N_s = -0.18 \cdot N \cdot S^2 + 0.38 \cdot N \cdot S + 0.02 \cdot N + 0.8 \quad (4)$$

We verify the formula in Table 5, where the number of shields given by the formula and that obtained by the SINO/NB- $k$  program are compared. As shown in this table, the difference between the formula and



N	sensitivity rate = 30%		sensitivity rate = 50%		sensitivity rate = 70%	
	estimation result	SINO/NB- <i>k</i> solution	estimation result	SINO/NB- <i>k</i> solution	estimation result	SINO/NB- <i>k</i> solution
16	2.7	3	3.4	4	4	4.4
32	4.6	3.0	6.1	6.4	7.2	7.6
64	8.3	8.4	11.4	11.6	13.5	14.2

Table 5: Comparison between the number of shields estimated by the formula and that obtained by the SINO/NB-*k* program. Here the uniform sensitivity is assumed, and  $K_{thresh}$  is set to 1.0. The maximum difference in this table is less than 10.0%.

the SINO/NB-*k* program is less than 10%.<sup>1</sup> Note that we can tune the constant  $f$  in function (3) such that the computational value can give a desired lower or upper bound of the number of shields required by SINO solutions.

Our estimation method is able to handle different  $K_{thresh}$  values. We derive the following formula (5) for  $K_{thresh}=1.5$ :

$$N_s = -0.23 \cdot N \cdot S^2 + 0.37 \cdot N \cdot S + 0.02 \cdot N + 0.6. \quad (5)$$

We further verify the estimation in Table 6. As shown in this table, the estimation error is less than 10%. In addition, same as shown in [4], when the  $K_{thresh}$  increases, the number of shields needed by SINO solutions decreases.

N	sensitivity rate = 30%		sensitivity rate = 50%		sensitivity rate = 70%	
	estimation result	SINO/NB- <i>k</i> solution	estimation result	SINO/NB- <i>k</i> solution	estimation result	SINO/NB- <i>k</i> solution
16	2.4	2.2	3.4	3.4	4.1	4.2
32	3.7	3.6	4.8	5.0	6.2	5.7
64	6.3	6.0	8.1	8.4	10.5	10.2

Table 6: Comparison between the number of shields estimated by the formula and that obtained by the SINO/NB-*k* program. Here  $K_{thresh}=1.5$  and the uniform sensitivity is assumed. The maximum estimation error is 8.8%.

### 3.1.2 RLC Nets with Non-uniform Sensitivity Rates

Formulae (4) and (5) can be extended easily to the case with non-uniform sensitivity rates. When the sensitivity is not uniform, the number of shields is

$$N_s = -0.18 \cdot \sum_{i=1}^N S_i^2 + 0.38 \cdot \sum_{i=1}^N S_i + 0.02 \cdot N + 0.8 \quad (6)$$

<sup>1</sup>As we will see from the comparison results in the following sub-sections, the error between each estimation and the corresponding SINO/NB solution is always within 10%.

for  $K_{thresh} = 1.0$ , and is

$$N_s = -0.23 \cdot \sum_{i=1}^N S_i^2 + 0.37 \cdot \sum_{i=1}^N S_i + 0.02 \cdot N + 0.6 \quad (7)$$

for  $K_{thresh}=1.5$ , where  $S_i$  is the sensitivity rate for s-wire  $s_i$ . We verify the above two formulae in Tables 7 and 8. The maximum difference between the estimation and the SINO/NB solution is 7.4% and 8.7%, respectively for  $K_{thresh}=1.0$  and 1.5.

	distribution of non-uniform sensitivity rates (N=32)	estimation result	SINO/NB- $k$ solution
sample 1	10% × 1 + 30% × 1 + 50% × 5 + 60% × 5 + 70% × 13 + 80% × 6 + 90% × 1	6.6	6.6
sample 2	30% × 4 + 40% × 11 + 50% × 6 + 60% × 10 + 70% × 1	5.8	5.4
sample 3	20% × 1 + 30% × 6 + 40% × 6 + 50% × 8 + 60% × 5 + 70% × 3 + 80% × 2 + 90% × 1	5.9	5.8

Table 7: Comparison between the number of shields estimated by the formula and that obtained by the SINO/NB- $k$  program. Here  $K_{thresh}=1.0$ , and non-uniform sensitivity is assumed. The maximum estimation error is 7.4%.

	distribution of non-uniform sensitivity rates (N=32)	estimation result	SINO/NB- $k$ solution
sample 1	10% × 1 + 30% × 1 + 50% × 5 + 60% × 5 + 70% × 13 + 80% × 6 + 90% × 1	5.6	5.0
sample 2	30% × 4 + 40% × 11 + 50% × 6 + 60% × 10 + 70% × 1	5.4	4.6
sample 3	20% × 1 + 30% × 6 + 40% × 6 + 50% × 8 + 60% × 5 + 70% × 3 + 80% × 2 + 90% × 1	5.1	4.6

Table 8: Comparison between the number of shields estimated by the formula and that obtained by the SINO/NB- $k$  program. Here,  $K_{thresh}=1.5$  and the non-uniform sensitivity is assumed. The maximum error is 8.7%.

### 3.2 SPR/NB- $k$ Algorithm

A brute-force solution to the min-area SPR/NB- $k$  problem is to enumerate all possible P/G structures using the  $p$ -SINO/NB- $k$  algorithm, and then find the SPR/NB- $k$  solution with the minimum area. Using the newly developed formulae for pre-SINO/NB- $k$  estimation, we are able to propose the following two-phase SPR/NB- $k$  algorithm: in the first phase, we define a single regular P/G structure according to pre-SINO/NB- $k$  estimation; and in the second phase, we carry out  $p$ -SINO/NB- $k$  procedures and find the best SPR/NB- $k$  solution, around the limited neighborhood of the pre-defined P/G structure. This two-phase algorithm is expected to be much more efficient compared to the brute-force solution.

More specifically, we speculate in the first phase that the optimal P/G structure that leads to the minimum number of shields should have a pitch space ( $PS$ ) given by formula (8):

$$PS = \lceil K \cdot \frac{N}{N_s} \rceil \quad (8)$$

where  $N$  is the number of signal nets, and  $N_s$  is the number of shields used in optimal SINO/NB- $k$  solutions. Formulae from (4) to (7) for the SINO/NB- $k$  estimation are used to compute  $N_s$  according to different  $K_{thresh}$  values and whether the distribution of the sensitivity rates is uniform or non-uniform. Furthermore, we speculate that the coefficient  $K$  is insensitive to different experiment settings. This speculation will be verified in the experiments to be presented.

To achieve the best SPR/NB- $k$  solution in the second phase, we first apply the  $p$ -SINO/NB- $k$  algorithm to assign signal nets into routing tracks and insert necessary g-wires (movable shields) with respect to the regular P/G structure defined by the pitch space given in formula (8). We call the resulting SPR/NB- $k$  solution the best among the  $0$ -order neighborhood (in short, *best of 0-neighbor*). We may then apply the  $p$ -SINO/NB- $k$  algorithm with respect to two extra P/G structures defined by pitch spaces  $(PS + 1)$  and  $(PS - 1)$ , respectively. We denote the best solution among these three pitch spaces  $(PS + 1)$ ,  $PS$ , and  $(PS - 1)$  as *the best of the first-order neighborhood* (in short, *best of 1st-neighbor*). Similarly, we may have the best of 2nd-neighbor, 3rd-neighbor, and etc.. We proceed to show in the next sub-section that searching only the first-order neighborhood is capable of achieving the min-area SPR/NB- $k$  solution.

### 3.3 Experimental Results

$K_{thresh}$	sensitivity rate	P/G pitch size		total shields/total g-wires			
		estimated value	optimal value	best of 0-neighbor	best of 1st-neighbor	best of 2nd-neighbor	best of 3rd-neighbor
1.0	30%	13	12	6.6/3.6	6.2/2.2	6.2/2.2	6.2/2.2
	40%	11	11	7.4/3.4	7.4/3.4	7.4/3.4	7.4/3.4
	50%	10	9	9.0/5.0	8.2/3.2	8.2/3.2	8.2/3.2
	60%	9	8	10.8/5.8	10.0/4.0	10.0/4.0	10.0/4.0
	70%	8	8	12.2/6.2	11.4/5.4	11.4/5.4	11.4/5.4
1.5	30%	14	13	6.4/3.4	5.8/2.8	5.8/2.8	5.8/2.8
	40%	12	12	6.4/2.4	6.4/2.4	6.4/2.4	6.4/2.4
	50%	11	11	7.0/3.0	7.0/3.0	7.0/3.0	7.0/3.0
	60%	10	10	8.0/4.0	8.0/4.0	8.0/4.0	8.0/4.0
	70%	9	9	9.8/4.8	9.8/4.8	9.8/4.8	9.8/4.8

Table 9: Summary of SPR/NB- $k$  solution for 48 signal nets with uniform sensitivity rates. In each cell of column 5-8 in the table, the first value is the total number of shields, and the second value is the total number of g-wires.

We apply our two-phase SPR/NB- $k$  algorithm to four sets of examples: one set of example has 48 nets with uniform sensitivity rates ranging from 30% to 70%, and the other three sets contains non-uniform sensitivity samples from Table 7. For each example, we still use two different  $K_{thresh} = 1.0$  and 1.5, respectively. We

$K_{thresh}$		P/G pitch size		total shields/total g-wires			
		estimated value	optimal value	best of 0-neighbor	best of 1st-neighbor	best of 2nd-neighbor	best of 3rd-neighbor
1.0	sample 1	9	8	7.8/4.8	7.2/3.2	7.2/3.2	7.2/3.2
	sample 2	10	10	5.6/2.6	5.6/2.6	5.6/2.6	5.6/2.6
	sample 3	10	9	6.2/3.2	5.8/2.8	5.8/2.8	5.8/2.8
1.5	sample 1	10	10	5.6/2.6	5.6/2.6	5.6/2.6	5.6/2.6
	sample 2	11	10	5.8/3.8	5.0/2.0	5.0/2.0	5.0/2.0
	sample 3	11	10	5.4/3.4	4.8/1.8	4.8/1.8	4.8/1.8

Table 10: Summary of SPR/NB- $k$  solution for 32 signal nets with non-uniform sensitivity rates. In each cell of column 5-8 in the table, the first value is the total number of shields, and the second value is the total number of g-wires.

estimate the pre-routing area via formulae from (4) to (7), then define the regular pitch space according to formula (8), and finally carry out  $p$ -SINO/NB- $k$  procedures to find SPR/NB- $k$  solutions as the best of 0-neighbor, 1st-neighbor, 2nd-neighbor, and 3rd-neighbor, respectively.

We present the total number of shields and g-wires in Tables 9 and 10, respectively for the uniform sensitivity case and the non-uniform sensitivity case. As shown in all these experiments, the best of 1st-neighbor is also the best of 3rd-neighbor. Further, our experiments also show that a neighborhood higher than third-order does not lead to a better solution. Therefore, our two-phase SPR/NB- $k$  algorithm is able to can find the optimal P/G structure and routing solution by simply searching the first-order neighborhood of the estimated pitch size given by formula (8). In addition, the total g-wires in all experiments are fewer than the total P/G wires, as required in our problem formulation. Moreover, as we speculated, the coefficient  $K$  can be set as a constant (=1.70 in all experiments here).

Based on all these experiments, we summarize our two-phase SPR/NB- $k$  algorithm in Figure 3 where the min-area SPR/NB- $k$  solution is guaranteed by only searching the first-order neighborhood of the pre-defined P/G structure.

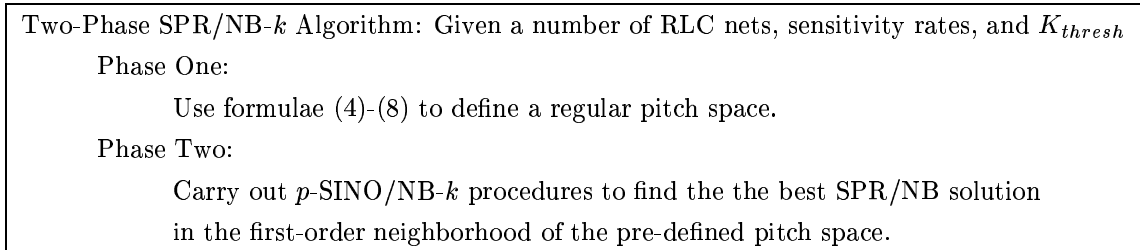


Figure 3: Two-Phase SPR/NB- $k$  Algorithm

## 4 Conclusions and Discussions

For a number of coupled RLC signal nets, we have formulated the min-area simultaneous signal and power routing (SPR/NB) problem satisfying the given noise bound under the  $K_{eff}$  model. Further, we have developed

a set of formulae to estimate the total numbers of shields needed by simultaneous shield insertion and net ordering (SINO) solutions, and have proposed a two-phase solution to the SPR/NB problem: in the first phase, we define a regular P/G structure based on the above interconnect estimation; and in the second phase,  $p$ -SINO/NB- $k$  procedures are executed to achieve the best solution for the simultaneous signal and power routing problem by searching the first-order neighborhood of the estimated optimal P/G structure. Experimental results have shown that our SPR/NB- $k$  solution satisfies the given noise bound under the  $K_{eff}$  model, and needs fewer g-wires than P/G wires.

As described in Section 2, the explicit RLC noise voltage model proposed in [3] is more general and accurate than the  $K_{eff}$  model. Our ongoing work extends the interconnect estimation, and the formulation and solution to the SPR/NB problem from the  $K_{eff}$  model to the explicit RLC noise model. Specifically, we are studying the following new  $p$ -SINO/NB- $v$  problem:

**Formulation 5** (*Optimal  $p$ -SINO/NB- $v$  problem*): For a given placement  $P$  with pre-routed P/G structure, find a new placement  $P'$  with the minimum area by simultaneous shield (g-wire only) insertion and net re-ordering such that the peak noise of any wire  $s_i$  in  $P'$  satisfies the given explicit noise constraints for wire  $s_i$ .

Same as [3], we apply the table-based partial inductance model, inductance screening rule, and higher-order RLC noise model. Based on the solution to the  $p$ -SINO/NB- $v$  problem, we are also studying the following new SPR/NB problem with respect to the explicit RLC noise model:

**Formulation 6** (**min-area SPR/NB- $v$  problem**) For given signal nets and RLC noise constraint, the min-area SPR/NB- $v$  problem decides a regular P/G structure, assigns signal nets to tracks, and insert necessary movable shields, such that the resulting solution has a minimum area under the given noise bound, and has g-wires fewer than P/G wires.

Preliminary results show that the frameworks proposed in this paper for the  $p$ -SINO/NB- $k$  and SPR/NB- $k$  problems are still applicable to the new  $p$ -SINO/NB- $v$  and SPR/NB- $v$  problems. These preliminary results, together with further development will be made available at the web site <http://eda.ece.wisc.edu>. In addition, we plan to incorporate our SPR/NB- $v$  formulation into a global router with consideration of RLC signal integrity for both signal and power nets. We will explore optimal wire sizing and spacing, and the placement of decoupling capacitance in the context of our SPR problem.

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